

Linear Voltage Regulators

Fundamental Theory of PMOS Low-Dropout Voltage Regulators

Abstract

Most linear modern linear regulators use a PMOS architecture. This application note explains the key characteristics of a PMOS Low-Dropout Voltage Regulator (LDO) and the theory behind it.

1. Fundamentals

A voltage regulator is a constant voltage source that adjusts its internal resistance to any occurring changes of load resistance to provide a constant voltage at the regulator output. The internal resistance of a constant voltage source (Figure 1) must be significantly smaller than the external load resistor ($R_{IN} \ll R_L$) to ensure a constant output voltage over a certain range of load.

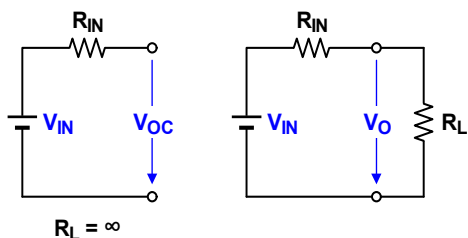


Figure 1. Constant-Voltage Source

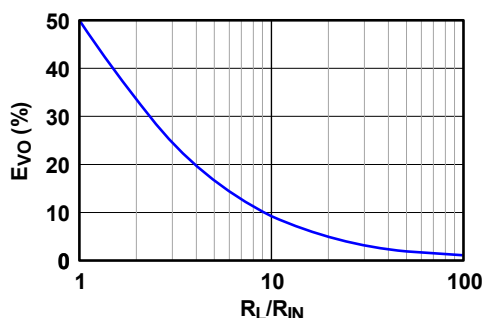


Figure 2. Output-Voltage Error vs Load Resistance

The output voltage of a voltage source under load condition is calculated with:

$$(EQ. 1) \quad V_O = V_{IN} \cdot \frac{R_L}{R_{IN} + R_L}$$

Under the no-load condition ($R_L = \infty$), the open-circuit output voltage (V_{OC}) is the maximum possible output voltage, which is equal to the input voltage: $V_{OC} = V_{IN}$. As the load increases, the output voltage drops from its maximum value and introduces an output-voltage error, E_{VO} . This error is defined as the percentage difference between V_{OC} , the output voltage under no-load condition, and V_O , the output voltage under load condition:

$$(EQ. 2) \quad E_{VO} = \frac{V_{OC} - V_O}{V_{OC}}$$

When replacing V_{OC} with V_{IN} and substituting V_O with Equation 1, the output voltage error is expressed through the resistor ratio of R_{IN} to R_L :

$$(EQ. 3) \quad E_{VO} = \frac{R_{IN}}{R_{IN} + R_L}$$

A plot of the voltage error over a series of R_L/R_{IN} ratios confirms that the output voltage error, E_{VO} , increases with decreasing load resistance R_L , as shown in Figure 2.

To minimize the error, we need a circuit that senses any occurring load changes and, using some kind of feedback, adjusts a variable internal resistor to keep a constant ratio of internal-resistance to load resistance, as described by Equation 4.

(EQ. 4) $R_{IN} = k \cdot R_L$

When the relationship described in [Equation 4](#) is true, R_{IN} must follow R_L in a linear relation, as expressed by [Equation 4](#). The corresponding equivalent circuit is shown in [Figure 3](#).

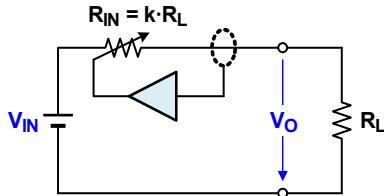


Figure 3. Linear Relation Between R_{IN} and R_L

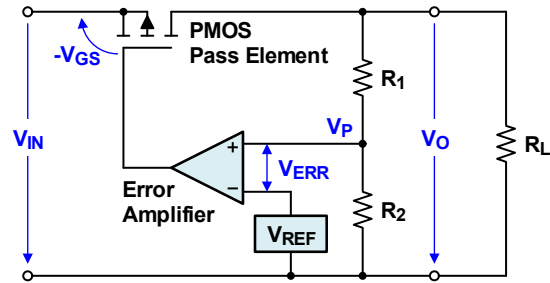


Figure 4. Basic Linear-Voltage Regulator

An electronic circuit that achieves this relationship by adjusting the variable input resistance is basically a linear-voltage regulator ([Figure 4](#)). Its functional building blocks are discussed in the following sections.

1.1 Voltage Reference, V_{REF}

The voltage reference is the foundation of all regulators. This reference is of the band-gap-type, which has the ability to operate at low supply voltages while providing sufficient accuracy and thermal stability to meet the less-stringent performance requirements of regulators. Bandgap references typically have an initial error of 0.5% to 1.0% and a temperature coefficient of 25ppm/°C to 50ppm/°C.

1.2 Error Amplifier

The error amplifier senses a scaled-down version of the output, $V_P = V_O \cdot R_2 / (R_1 + R_2)$, compares it against the reference voltage ($V_P = V_{REF}$), and adjusts V_O using the series-pass element to the value required to drive the error signal ($V_{ERR} = V_P - V_{REF}$) as close as possible to zero. Setting $V_{REF} = V_P$ and solving for V_O yields [Equation 5](#):

(EQ. 5)
$$V_O = V_{REF} \cdot \left(1 + \frac{R_1}{R_2} \right)$$

This calculation holds true only if V_{IN} is sufficiently high to keep the error amplifier and the pass element from saturating.

1.3 Feedback Network

The feedback network scales V_O to a value suitable for comparison against V_{REF} by the error amplifier. Because V_{REF} is fixed, the only way to program the value of V_O is by adjusting the ratio R_1 / R_2 .

1.4 Pass Element

The series-pass element boosts the output-current capability of the error amplifier to the higher levels required by the load. This process involves transferring large currents from the source, V_{IN} , to the load under the low-power supervision of the error amplifier. A suitable pass element to carry out this task is a PMOS enhancement FET.

A PMOS FET has the two p-islands for the source and the drain terminals embedded in an n-substrate ([Figure 5](#)). The substrate is connected to the source, which usually has the most positive potential. The drain receives the most negative potential.

As the PMOS name indicates, the device uses p-type conductivity, which is established by applying a voltage to the gate that is negative relative to the source. The holes, which are the minority carriers in the n-substrate, are attracted by the negative gate electrode. Moving towards the upper region between the two p-islands, the holes

now become free-charge carriers, establishing a p-conductive bridge between source and drain. This way, the conductivity of the bridge and the drain current I_D , are controlled by the gate-source voltage, V_{GS} .

Because this type of FET enhances its conductivity with increasing V_{GS} , it is called an enhancement or normally-off type (Figure 6).

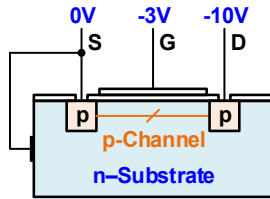


Figure 5. PMOS FET Basic Structure

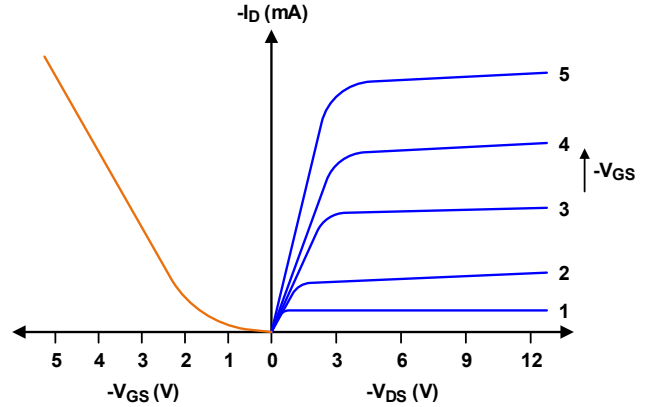


Figure 6. PMOS FET Input and Output Characteristics

2. Regulator Sequence

This section describes the regulation sequence when R_L drops as shown in Figure 9. Figure 7 depicts how the regulation sequence described relates to the internal LDO blocks.

When the load resistance drops, the output voltage falls from V_{O1} to V_{O2} , and the voltage across the pass element rises from $-V_{DS1}$ to $-V_{DS2}$. V_P (the scaled-down version of V_O) falls significantly below V_{REF} causing the gate-source voltage to jump from $-V_{GS1}$ to $-V_{GS2}$.

The PMOS FET now conducts harder, increasing the output current from I_{O1} to I_{O2} . The output voltage and, by virtue of V_P , the error voltage starts to recover. The gate voltage increases gradually to $-V_{GS3}$, therefore causing the increased output current I_{O3} to generate an output voltage V_O . When this output voltage is scaled down using R_1 and R_2 , the result is a zero-error voltage $V_{ERR} = 0$.

The output characteristic shown in Figure 8 confirms the regulation sequence. When R_L drops, the PMOS FET operating point jumps from P_1 to P_2 and then regulates to P_3 .

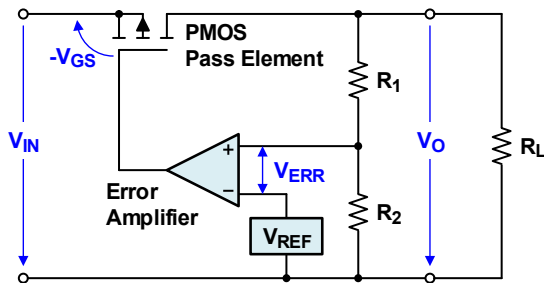


Figure 7. Regulator Block Diagram

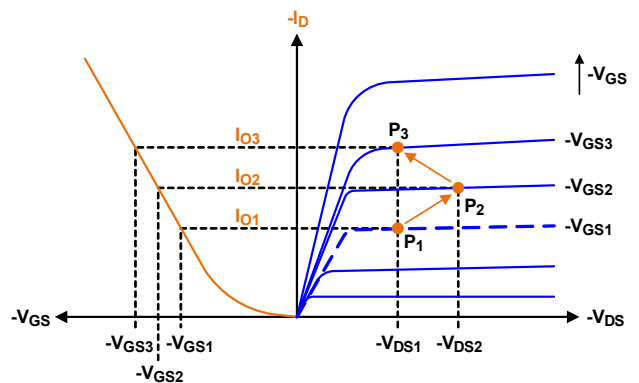


Figure 8. PMOS Input/Output Characteristic

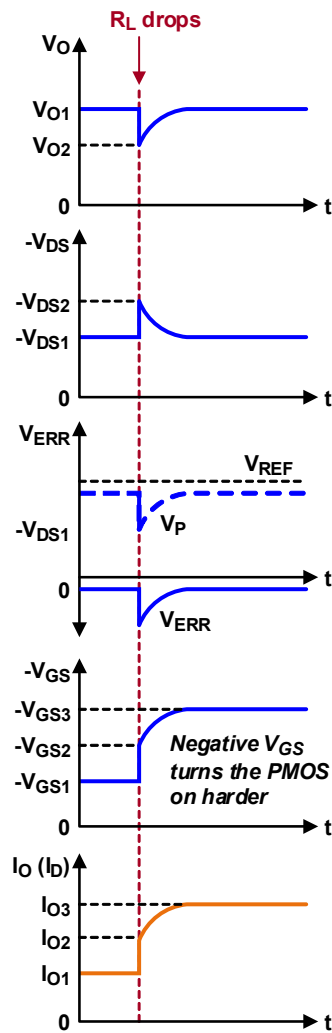


Figure 9. Regulation Sequence when R_L Drops

For a given quiescent point, P_3 , where the output voltage is stabilized (that is, V_{OUT} and V_{DS} are constant), the corresponding output current, I_{OUT3} , is defined through [Equation 6](#):

$$(EQ. 6) \quad I_{OUT3} = \frac{V_{DS}}{R_{IN}} = \frac{V_O}{R_L}$$

Then, solving for R_{IN} yields:

$$(EQ. 7) \quad R_{IN} = R_L \cdot \frac{V_{DS}}{V_O}$$

With $k = V_{DS}/V_O$, [Equation 7](#) provides the linear resistance relation required by a linear voltage regulator.

3. Revision History

Rev.	Date	Description
1.00	May.21.20	Initial release

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